

Automatic Control (2)



By



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ELECTRICAL
ENGINEERING AND
CONTROL PROGRAM



كلية الهندسة بشبرا

FACULTY OF ENGINEERING AT SHOUBRA



Lecture (4)



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Course Title: Automatic Control (2)

Course Code: EEC 415

Prerequisites: EEC224 Signals and Systems

Study Hours: 3 Cr. hrs.

= [2 Lect. + 0 Tut + 3 Lab]





Assessment:

Final Exam: 40%.

Midterm: 30%.

Quizzes: 10%.

Home assignments and Reports: 10%.

MATLAB Mini Project: 10%.

Textbook:

- 1- K. Ogata, Modern Control Engineering, Pearson, 5th. Ed., 2009.
- 2- Nise, N. S. "Control System Engineering", 7th edition, John Wiley & Sons Ltd., UK, 2016.
- 3- F. Golnaraghi and B. C. Kuo, "Automatic control Systems", 10th ed., John Wiley & Sons, Inc. 2017.
- 4- Andrea Bacciotti, "Stability and Control of Linear Systems" Volume 185, Springer, 2019.



Course Description

- Compensation in control systems, lead, lag, and lead-lag phase compensation in frequency domain,
- State model of linear systems using physical variables, state space representation using phase variables, state space representation, using canonical variables, properties of transition matrix and solution of state equation,
- Poles, zeros, eigen values and stability in multivariable system,
- Introduction to nonlinear control systems, describing function method, nature and stability of limit cycle.

Analysis & Design of Control Systems using Frequency Response

Controller

Input: $A \sin \omega t$

Output: $\hat{A} \sin(\omega t + \phi)$

\hat{A}/A is the normalized amplitude ratio (AR)

ϕ is the phase angle, response angle (RA)

AR and ϕ are functions of ω

Assume $G(s)$ known and let

$$s = j\omega \quad G(j\omega) = K_1 + K_2 j$$

$$|G| = AR = \sqrt{K_1^2 + K_2^2}$$

$$\phi = \angle G = \arctan \frac{K_2}{K_1}$$

Ideal PID Controller.

$$G_c(s) = K_c \left(1 + \frac{1}{\tau_I s} + \tau_D s \right)$$

Series PID Controller. The simplest version of the series PID controller is

$$G_c(s) = K_c \left(\frac{\tau_I s + 1}{\tau_I s} \right) (\tau_D s + 1)$$

Series PID Controller with a Derivative Filter. The series controller with a derivative filter was described in Chapter 8

$$G_c(s) = K_c \left(\frac{\tau_I s + 1}{\tau_I s} \right) \left(\frac{\tau_D s + 1}{\alpha \tau_D s + 1} \right)$$

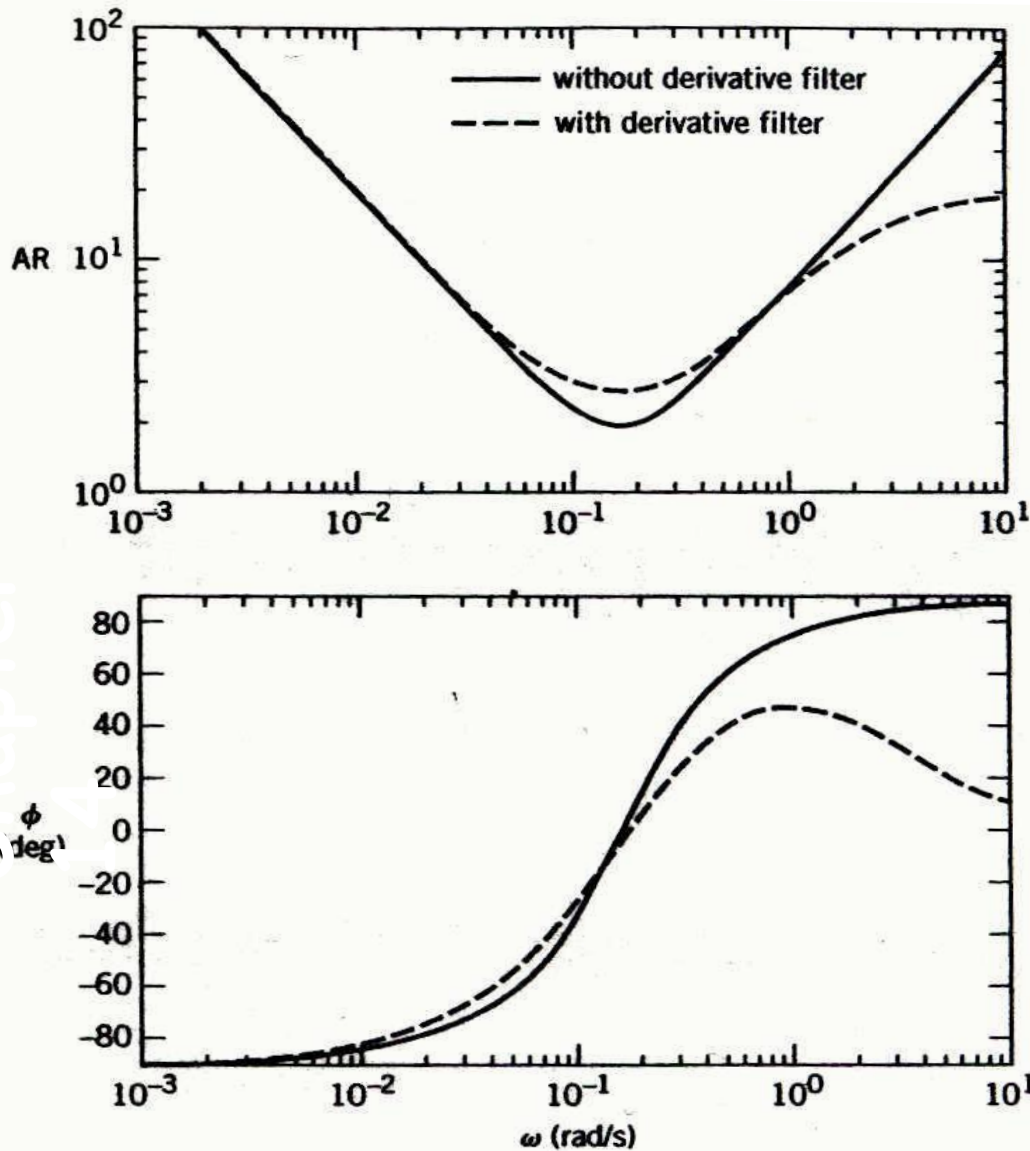


Figure Bode plots of ideal parallel PID controller and series PID controller with derivative filter ($\alpha = 1$).

Ideal parallel:

$$G_c(s) = 2 \left(1 + \frac{1}{10s} + 4s \right)$$

Series with Derivative Filter:

$$G_c(s) = 2 \left(\frac{10s + 1}{10s} \right) \left(\frac{4s + 1}{0.4s + 1} \right)$$

Advantages of FR Analysis for Controller Design:

1. Applicable to dynamic model of any order (including non-polynomials).
2. Designer can specify desired closed-loop response characteristics.
3. Information on stability and sensitivity/robustness is provided.

Disadvantage:

The approach tends to be iterative and hence time-consuming

-- interactive computer graphics desirable
(MATLAB)

Bode Plot Overview

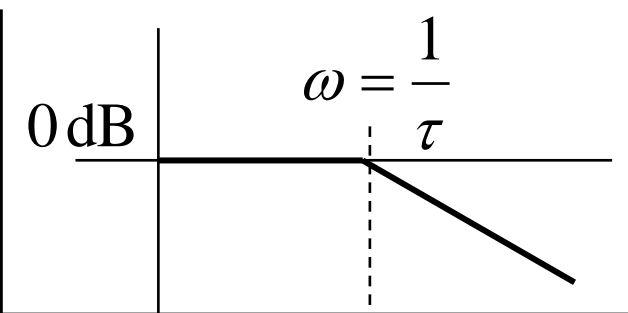
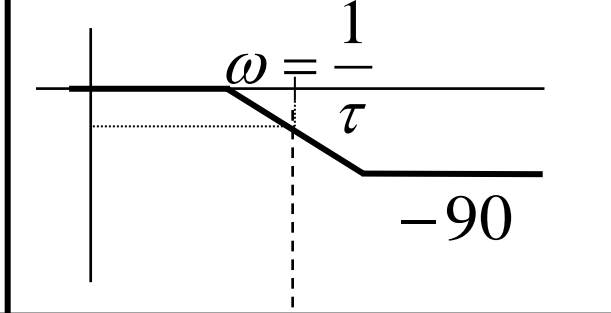
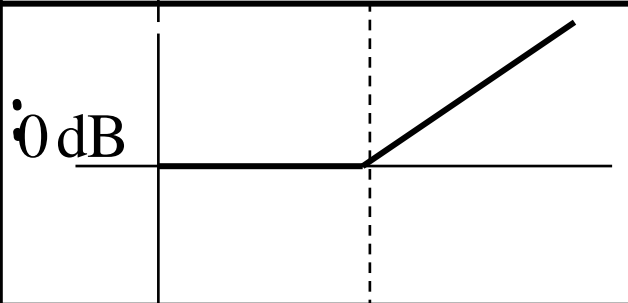
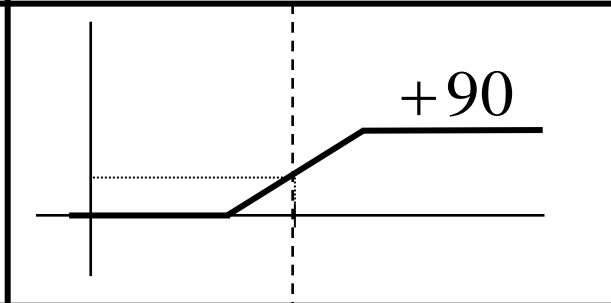
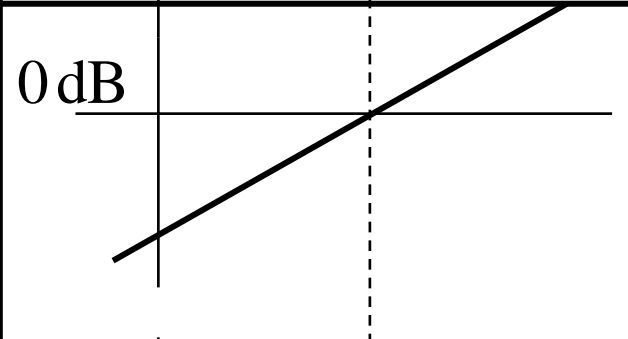
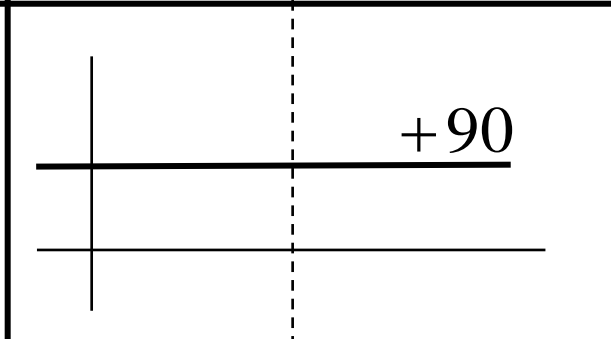
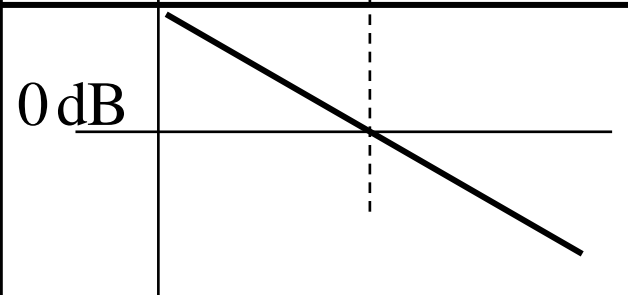
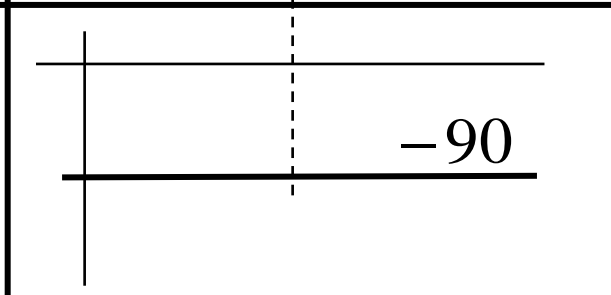
Technique for estimating a complicated transfer function (several poles and zeroes) quickly

$$H(\omega) = G_0(j\omega)^K \frac{(1 + j\omega\tau_{z1})(1 + j\omega\tau_{z2}) \cdots (1 + j\omega\tau_{zn})}{(1 + j\omega\tau_{p1})(1 + j\omega\tau_{p2}) \cdots (1 + j\omega\tau_{pm})}$$

Break frequencies :

$$\omega_i = \frac{1}{\tau_i}$$

Summary of Individual Factors

<p>Simple Pole:</p> $\frac{1}{1 + j\omega\tau}$	 <p>0 dB</p> <p>$\omega = \frac{1}{\tau}$</p>	 <p>$\omega = \frac{1}{\tau}$</p> <p>-90</p>
<p>Simple Zero:</p> $1 + j\omega\tau$	 <p>0 dB</p> <p>$\omega = \frac{1}{\tau}$</p>	 <p>+90</p>
<p>DC Zero:</p> $j\omega\tau$	 <p>0 dB</p>	 <p>+90</p>
<p>DC Pole:</p> $\frac{1}{j\omega\tau}$	 <p>0 dB</p>	 <p>-90</p>

Example

Consider the following transfer function

$$H(j\omega) = \frac{10^{-5} j\omega(1 + j\omega\tau_2)}{(1 + j\omega\tau_1)(1 + j\omega\tau_3)}$$

$\tau_1 = 100\text{ns}$
 $\tau_2 = 10\text{ns}$
 $\tau_3 = 100\text{ps}$

Break frequencies: invert time

$\omega_1 = 10\text{Mrad/s}$
constants

$\omega_2 = 100\text{Mrad/s}$

$\omega_3 = 10\text{Grad/s}$

$$H(j\omega) = \frac{\frac{j\omega}{10^5} \left(1 + j \frac{\omega}{\omega_2}\right)}{\left(1 + j \frac{\omega}{\omega_1}\right) \left(1 + j \frac{\omega}{\omega_3}\right)}$$

Breaking Down the Magnitude

Recall log of products is sum of logs

$$\begin{aligned} |H(j\omega)|_{\text{dB}} &= 20\log \left| \frac{\frac{j\omega}{10^5} (1 + j\frac{\omega}{\omega_2})}{(1 + j\frac{\omega}{\omega_1})(1 + j\frac{\omega}{\omega_3})} \right| \\ &= 20\log \left| \frac{j\omega}{10^5} \right| + 20\log \left| 1 + j\frac{\omega}{\omega_2} \right| \\ &\quad - 20\log \left| 1 + j\frac{\omega}{\omega_1} \right| - 20\log \left| 1 + j\frac{\omega}{\omega_3} \right| \end{aligned}$$

Let's plot each factor separately and add them graphically

Breaking Down the Phase

Since $\angle a \cdot b = \angle a + \angle b$

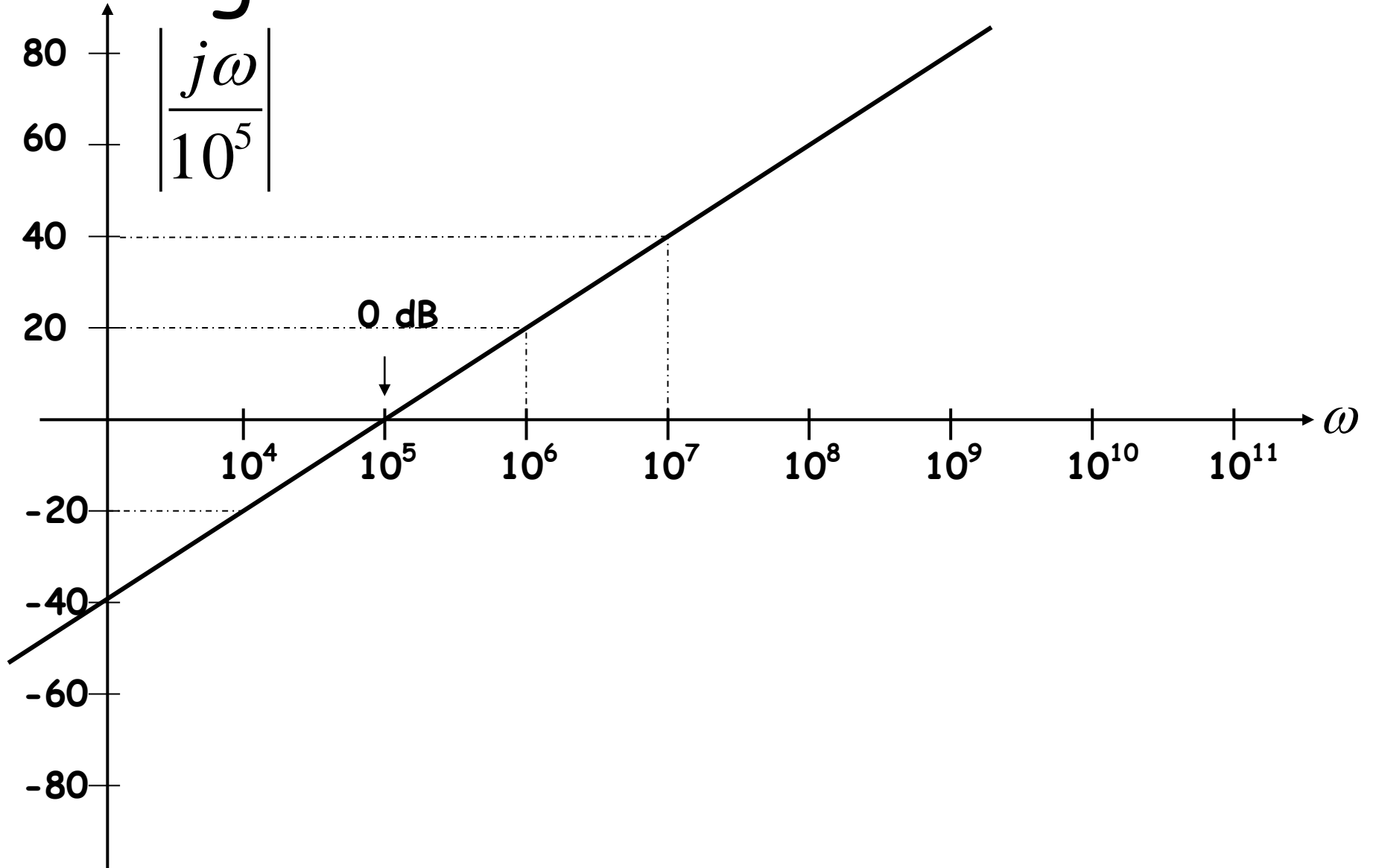
$$\angle H(j\omega) = \angle \frac{10^{-5} j\omega(1 + j\omega\tau_2)}{(1 + j\omega\tau_1)(1 + j\omega\tau_3)}$$

$$\angle H(j\omega) = \angle \frac{j\omega}{10^5} + \angle 1 + j \frac{\omega}{\omega_2}$$

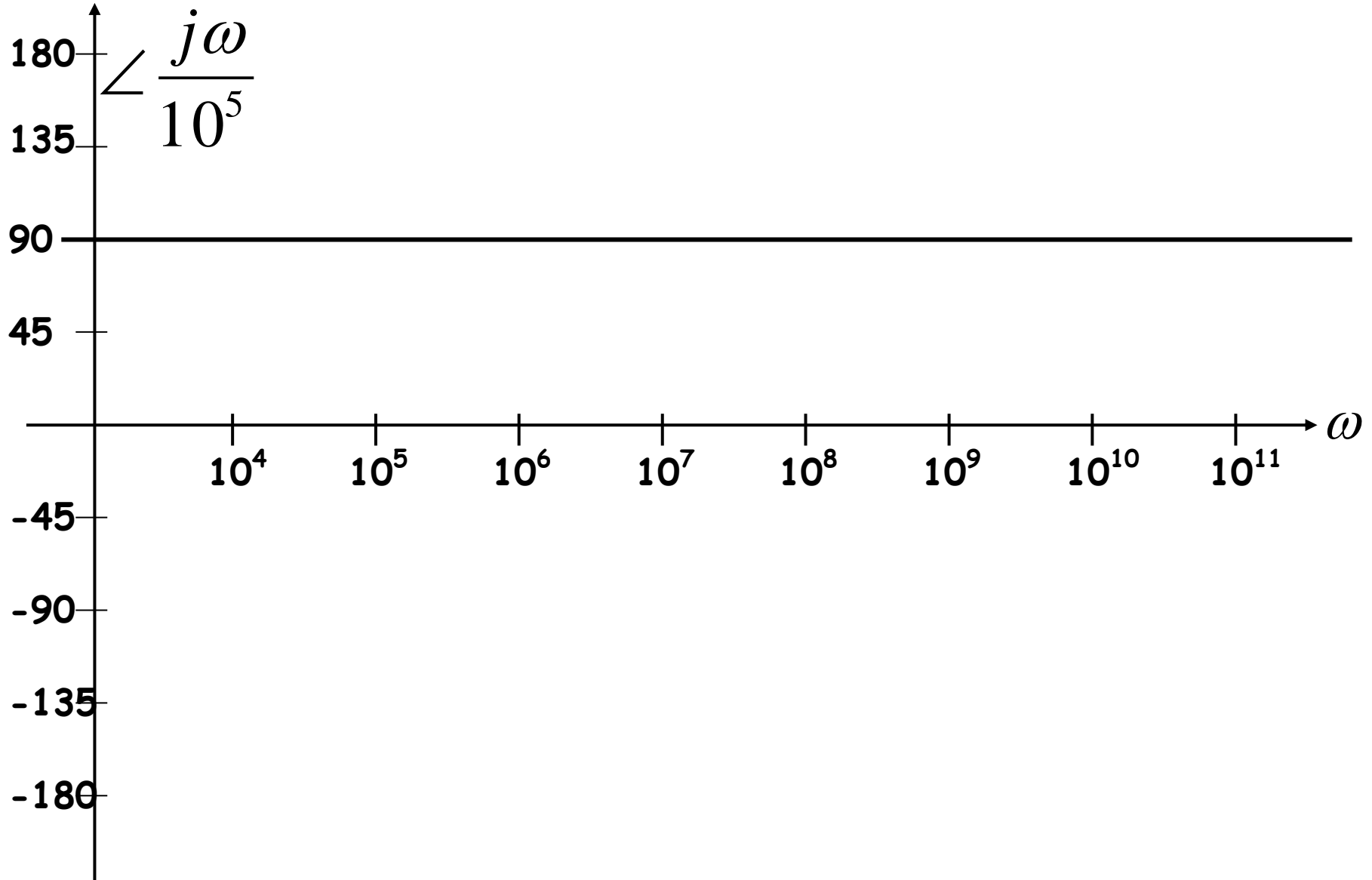
$$- \angle 1 + j \frac{\omega}{\omega_1} - \angle 1 + j \frac{\omega}{\omega_3}$$

Let's plot each factor separately and add them graphically

Magnitude Bode Plot: DC Zero

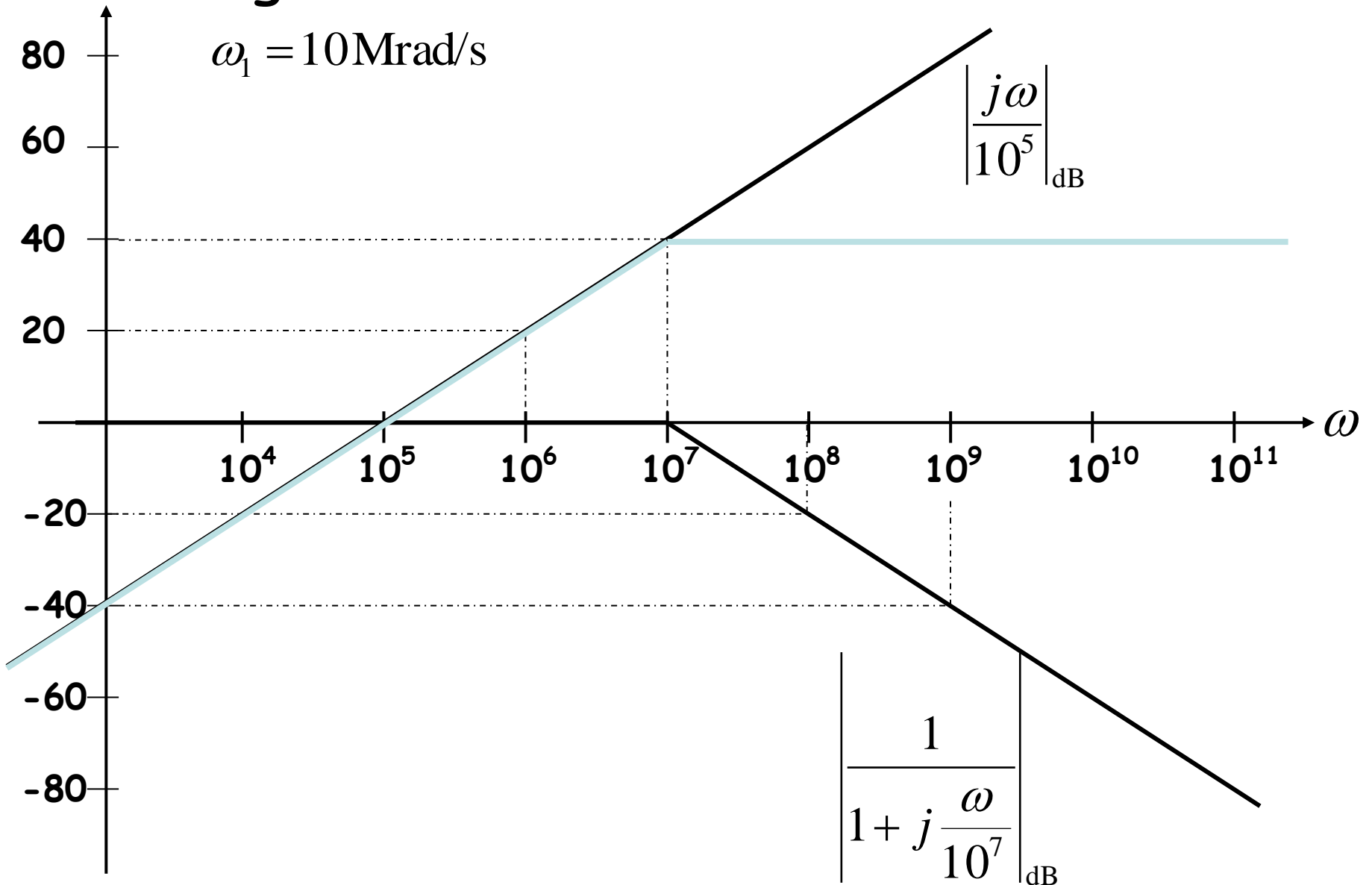


Phase Bode Plot: DC Zero

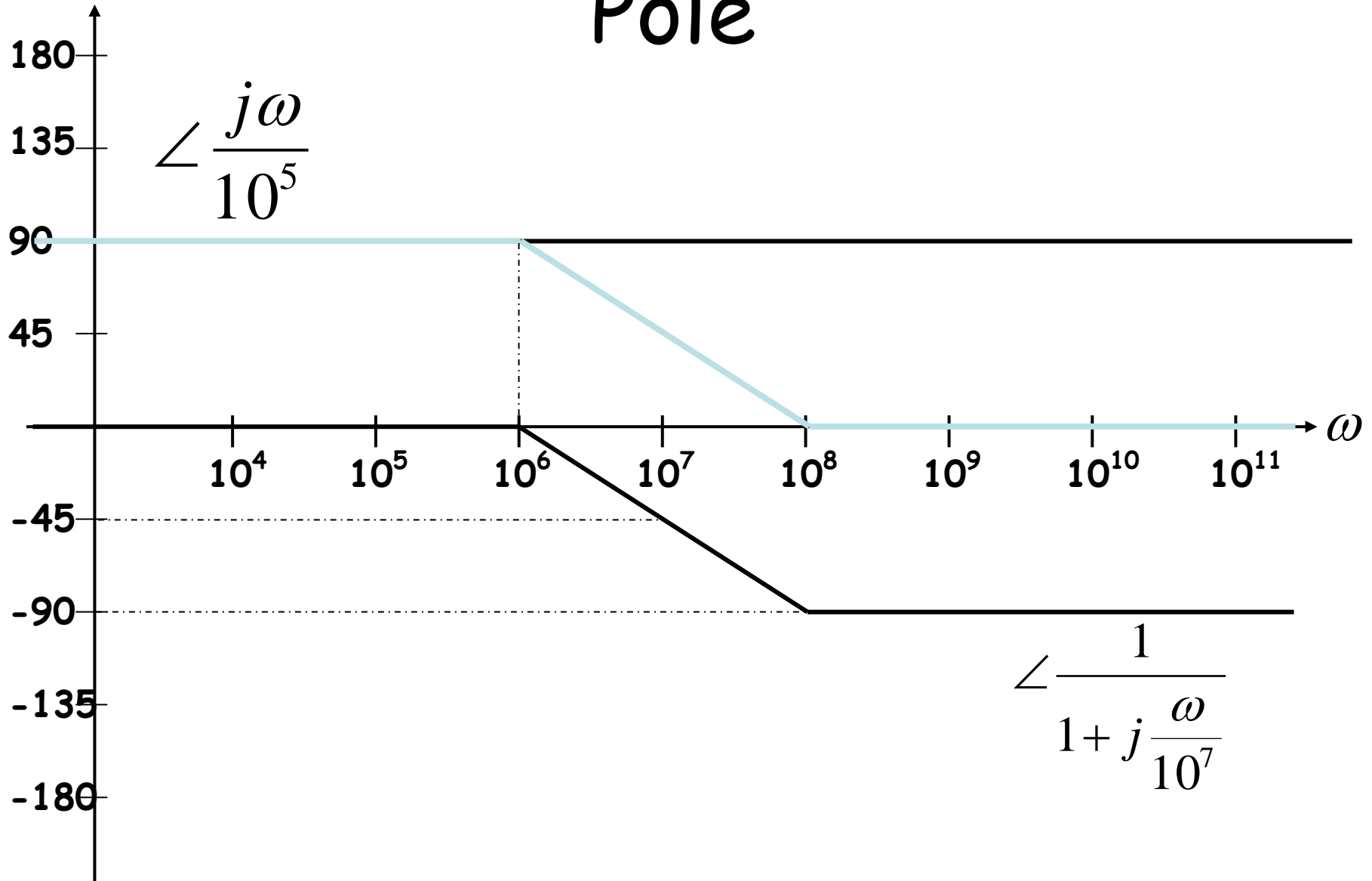


Magnitude Bode Plot: Add First Pole

$$\omega_1 = 10 \text{ Mrad/s}$$



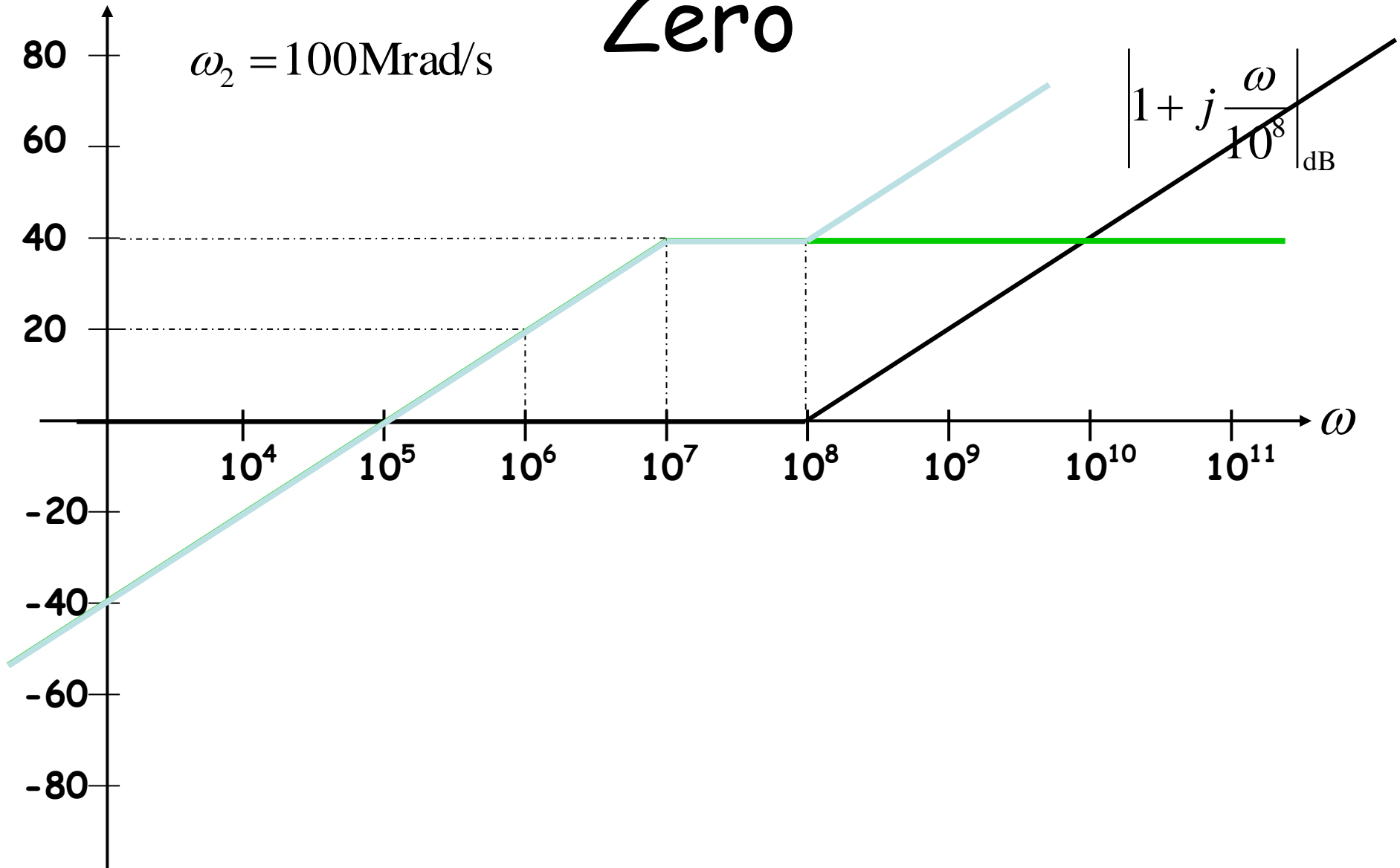
Phase Bode Plot: Add First Pole



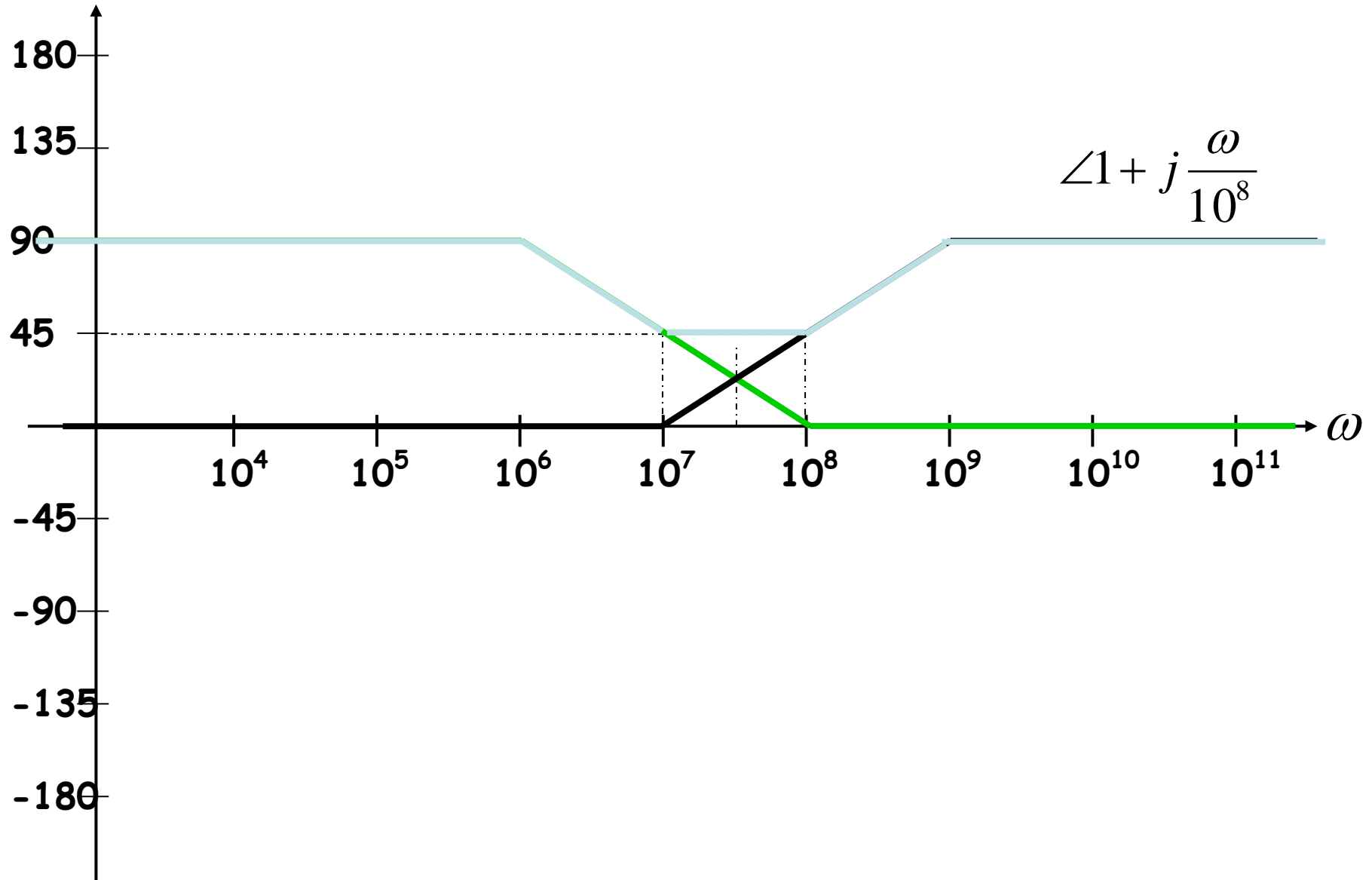
Magnitude Bode Plot: Add 2nd Zero

$\omega_2 = 100\text{Mrad/s}$

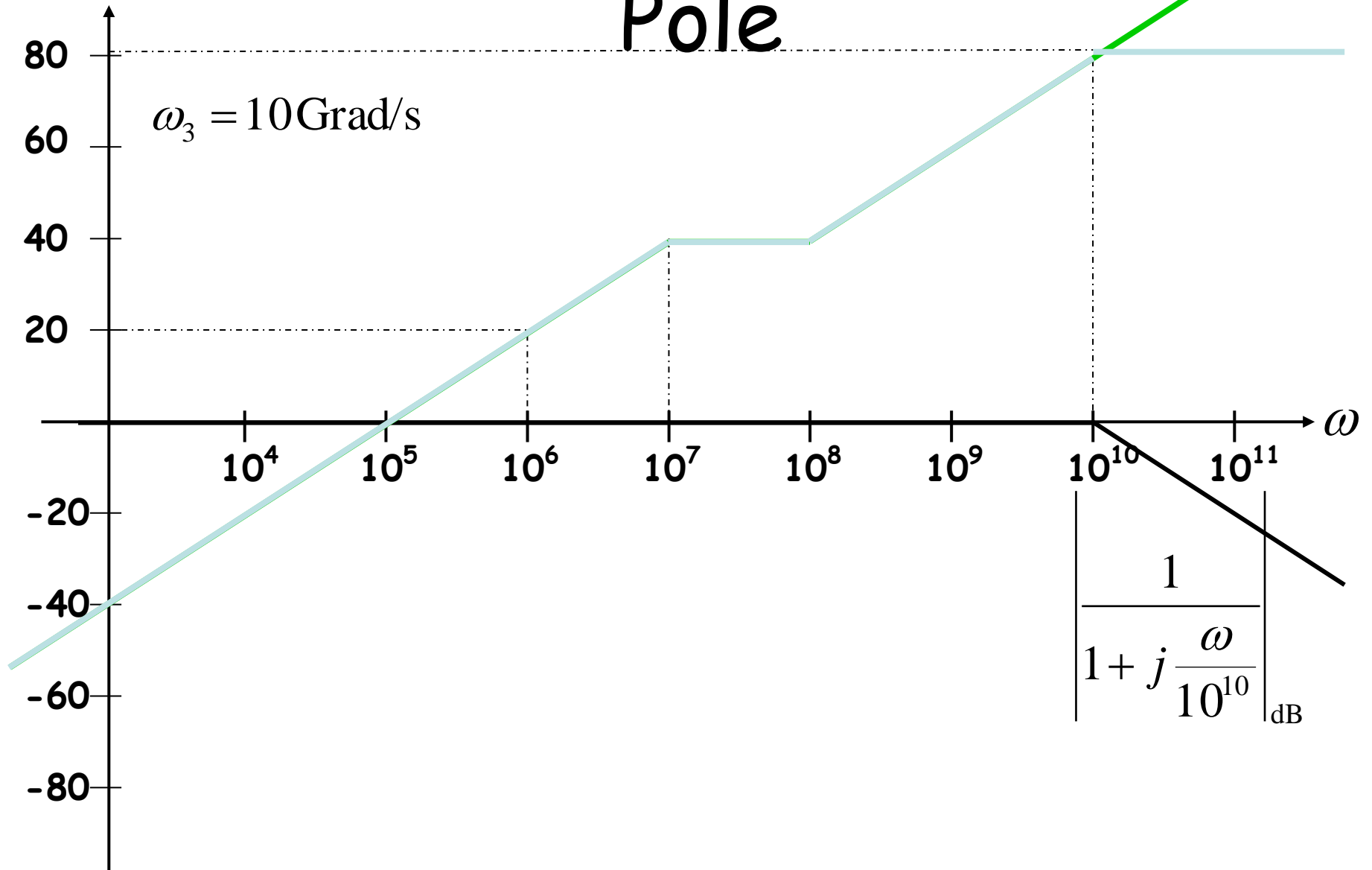
Zero



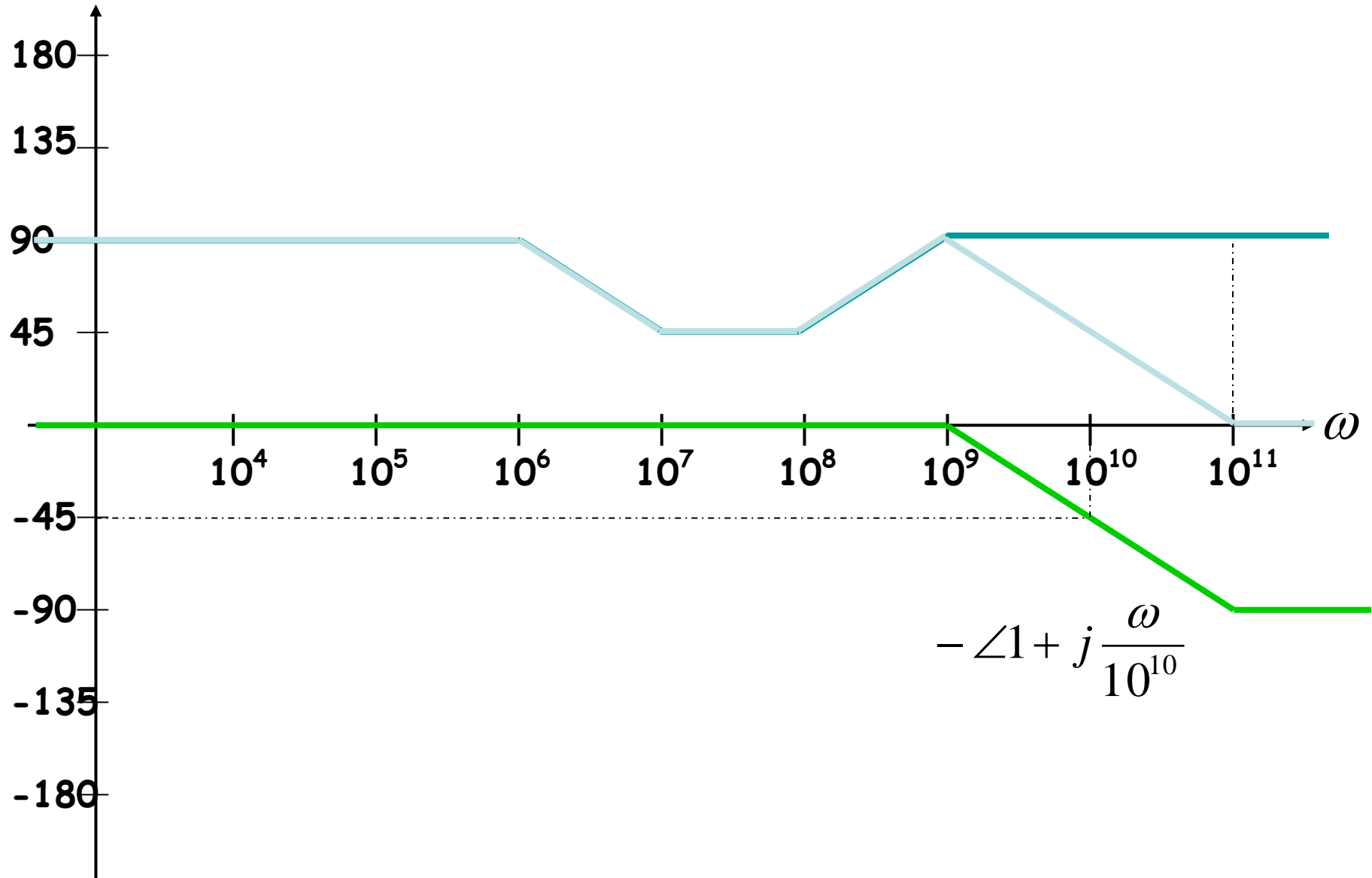
Phase Bode Plot: Add 2nd Zero



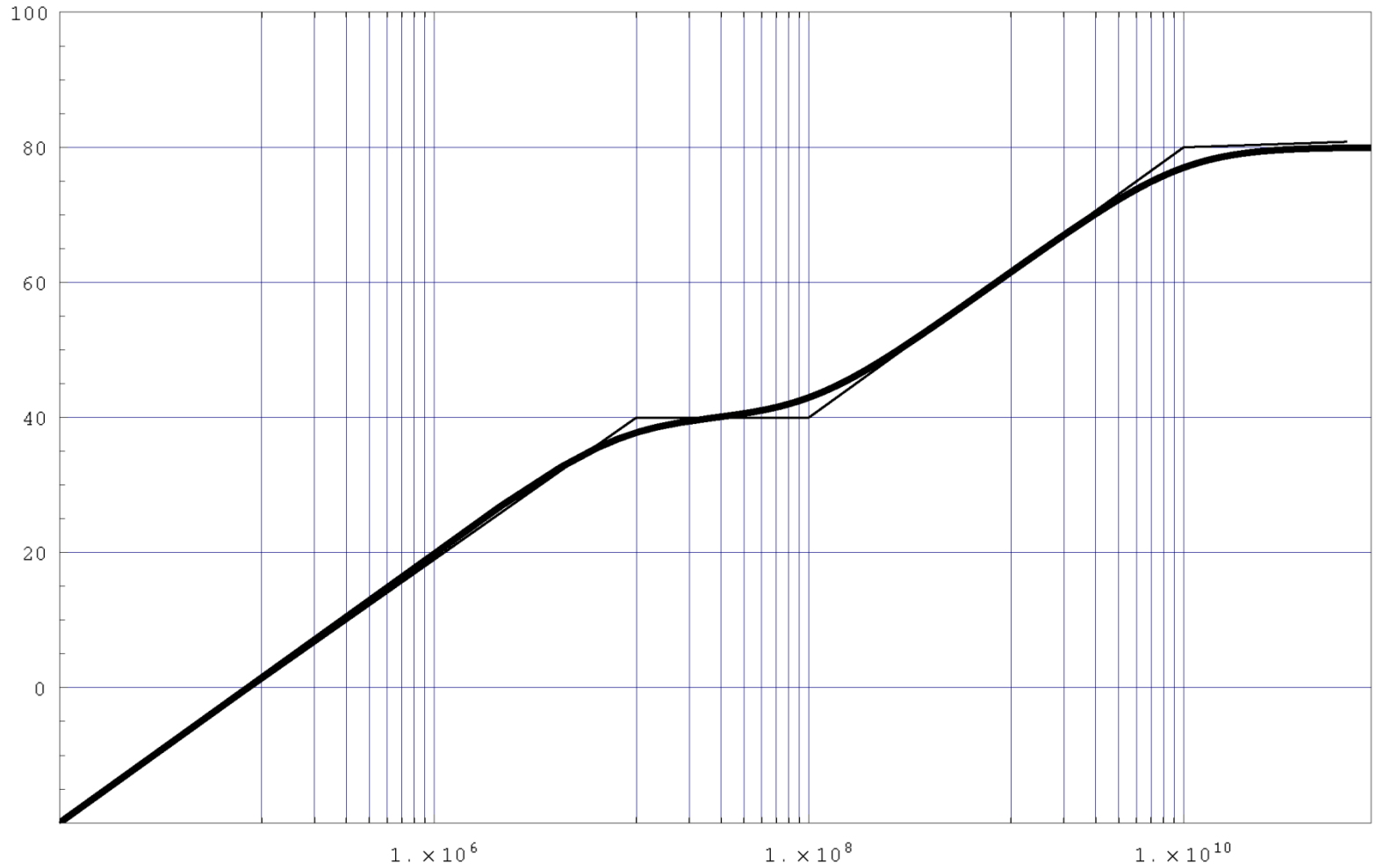
Magnitude Bode Plot: Add 2nd Pole



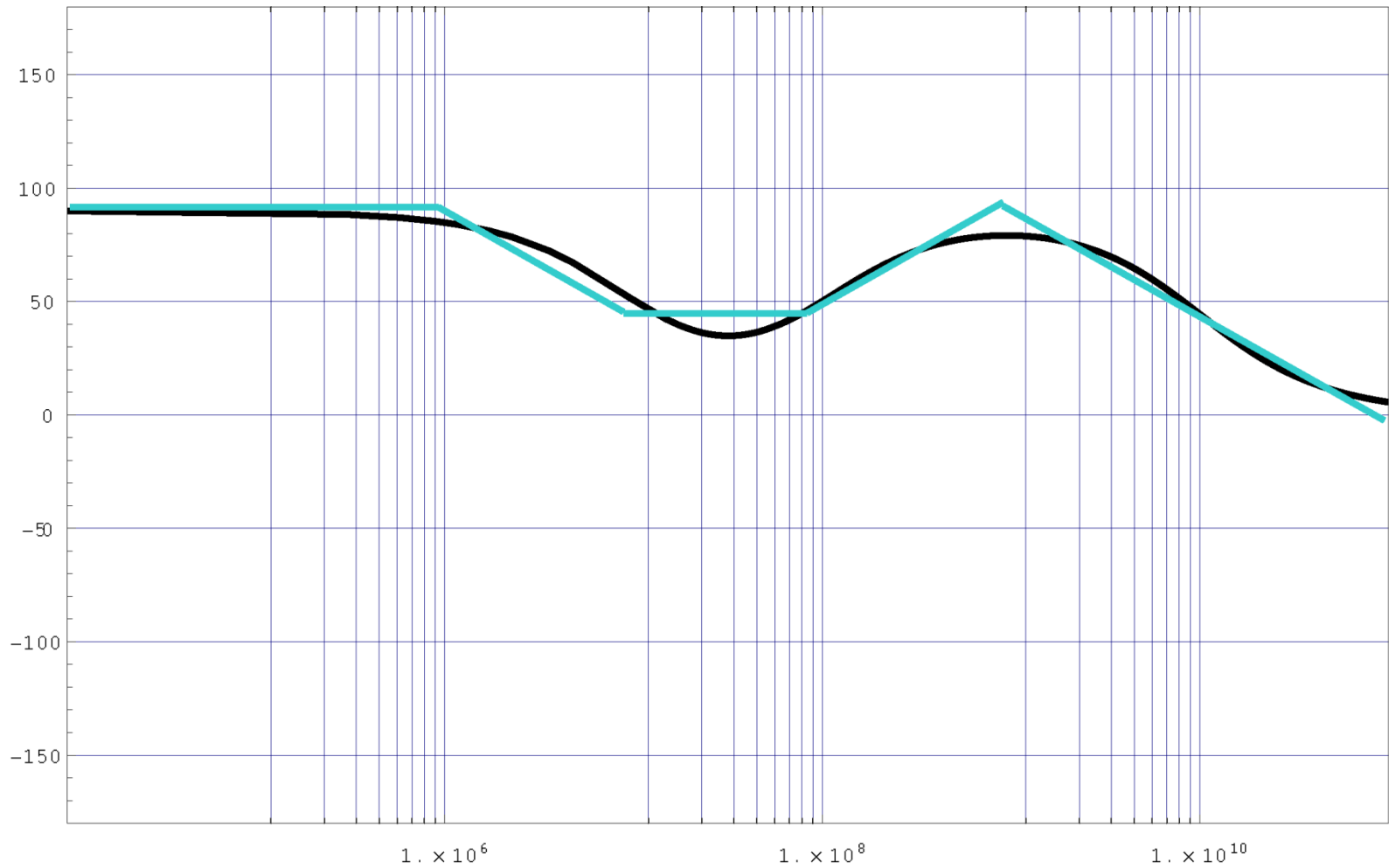
Phase Bode Plot: Add 2nd Pole



Comparison to "Actual" Mag Plot



Comparison to "Actual" Phase Plot



With Our Best Wishes
Automatic Control (2)
Course Staff

Thank You
For Your Attention



Mohamed Ahmed Ebrahim

Associate Prof. Dr. Mohamed Ahmed Ebrahim